

Family Name	Given Name	Student Number
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$\nabla \cdot \mathbf{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \quad \nabla \cdot \mathbf{D} = r_v \quad \oint_S \mathbf{D} \cdot d\mathbf{S} = Q_{encl}, \quad \int r \sin(ar) dr = \frac{1}{a^2} \sin(ar) - \frac{r}{a} \cos(ar)$

(1) (a) A spherical surface of radius 3mm is centered at $P(4m, 1m, 5m)$ in free space. Let $\mathbf{D} = x\mathbf{a}_x$ C/m². Find the net electric flux leaving the spherical surface. **(2 marks)**

Since \mathbf{D} is electric flux density, the flux leaving the surface is $\oint_S \mathbf{D} \cdot d\mathbf{S} = \int_V \nabla \cdot \mathbf{D} dv$. The last step uses divergence theorem. Using the equations given above, one could also use Gauss' law

$$\oint_S \mathbf{D} \cdot d\mathbf{S} = Q_{encl} = \int_V r_v dv = \int_V \nabla \cdot \mathbf{D} dv. \text{ Also from the equations given, } \nabla \cdot \mathbf{D} = \frac{\partial D_x}{\partial x} = 1$$

$$\therefore \oint_S \mathbf{D} \cdot d\mathbf{S} = 1 \times (\text{volume of sphere}) = \frac{4}{3} \pi (3 \times 10^{-3})^3 = 36\pi \times 10^{-9} \text{ C}. \text{ Note the units are Coulombs (C).}$$

(b) Find the electric field everywhere given an infinite cylinder of charge with **(3 marks)**

$$\begin{aligned} \rho_v &= 0 & \rho < 1\text{m}, \\ \rho_v &= 2\sin(2000\rho) & 1\text{m} < \rho < 1.5\text{m}, \\ \rho_v &= 0 & \rho > 1.5\text{m} \end{aligned}$$

Clearly, this problem is solved using Gauss' law. Due to symmetry, the fields are in the \mathbf{r} -direction. As done several times in class, the Gaussian surface will be a cylinder of radius r and length L . We need to worry about three cases, $r < 1$, $1 < r < 1.5$ and $r > 1.5$.

$$\text{Gauss' Law: } \oint_S \mathbf{D} \cdot d\mathbf{S} = Q_{encl}. \text{ Also, } \mathbf{D} = D_r \mathbf{a}_r \Rightarrow \oint_S \mathbf{D} \cdot d\mathbf{S} = D_r 2\pi r L$$

Case 1: $r < 1$. Since the charge density for $r < 1$ is zero, there is no charge enclosed within any surface. Therefore the flux density $\mathbf{D} = 0$ and $\mathbf{E} = 0$.

Case 3: $r > 1.5$. Now, the surface encloses all the charge within the length L .

$$\begin{aligned} Q_{encl} &= \int_V r_v dv = \int_0^L \int_0^{2\pi} \int_1^{1.5} 2\sin(2000\rho r') dr' d\phi dz' = 2\pi L \int_1^{1.5} 2\sin(2000\rho r') dr' \\ &= 4\pi L \left[\frac{1}{(2000\rho)^2} \sin(2000\rho r') - \frac{r'}{2000\rho} \cos(2000\rho r') \right] \Bigg|_{r'=1}^{r'=1.5} \end{aligned}$$

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$$Q_{encl} = 4\mathbf{p}L \left\{ \frac{1}{(2000\mathbf{p})^2} [\sin(3000\mathbf{p}) - \sin(2000\mathbf{p})] - \frac{1.5}{2000\mathbf{p}} \cos(3000\mathbf{p}) + \frac{1}{2000\mathbf{p}} \cos(2000\mathbf{p}) \right\}$$

Since $\sin(2n\mathbf{p}) = 0$ and $\cos(2n\mathbf{p}) = 1$ for integer n , $\sin(3000\mathbf{p}) = \sin(2000\mathbf{p}) = 0$, $\cos(3000\mathbf{p}) = \cos(2000\mathbf{p}) = 1$.

$$Q_{encl} = \frac{-0.5}{2000\mathbf{p}} 4\mathbf{p}L \Rightarrow D_r = \frac{-1}{(2000\mathbf{p})r}, \quad \mathbf{D} = \left[\frac{-1}{(2000\mathbf{p})r} \right] \mathbf{a}_r.$$

Case 2: $1 < r < 1.5$. Now, the Gaussian surface encloses only some of the charge.

$$\begin{aligned} Q_{encl} &= \int_V \mathbf{r}_v dv = \int_0^L \int_0^{2\mathbf{p}} \int_0^r 2\sin(2000\mathbf{p}r') dr' d\mathbf{f} dz' = 2\mathbf{p}L \int_1^r 2\sin(2000\mathbf{p}r') dr' \\ &= 4\mathbf{p}L \left[\frac{1}{(2000\mathbf{p})^2} \sin(2000\mathbf{p}r') - \frac{r'}{2000\mathbf{p}} \cos(2000\mathbf{p}r') \right] \Bigg|_{r'=1}^{r'=r} \\ &= 4\mathbf{p}L \left\{ \frac{1}{(2000\mathbf{p})^2} [\sin(2000\mathbf{p}r) - \sin(2000\mathbf{p})] - \frac{r}{2000\mathbf{p}} \cos(2000\mathbf{p}r) + \frac{1}{2000\mathbf{p}} \cos(2000\mathbf{p}) \right\} \\ &= 4\mathbf{p}L \left[\frac{\sin(2000\mathbf{p}r)}{(2000\mathbf{p})^2} - \frac{r}{2000\mathbf{p}} \cos(2000\mathbf{p}r) + \frac{1}{2000\mathbf{p}} \right] \end{aligned}$$

$$D_r = \frac{2}{r} \left[\frac{\sin(2000\mathbf{p}r)}{(2000\mathbf{p})^2} - \frac{r}{2000\mathbf{p}} \cos(2000\mathbf{p}r) + \frac{1}{2000\mathbf{p}} \right] \text{ and } \mathbf{D} = D_r \mathbf{a}_r.$$

SOLUTION

$$\begin{aligned} (2)(a) \quad V_A &= \frac{Q}{4\pi\epsilon_0 |\vec{r}_A - \vec{r}_B|} \quad \text{WITH } V=0 \text{ AT } \infty \text{ AS REF.} \\ &= \frac{200\pi\epsilon_0}{4\pi\epsilon_0 |(5\vec{a}_x + 6\vec{a}_y + 7\vec{a}_z) - (3\vec{a}_x - 1\vec{a}_y + 2\vec{a}_z)|} \\ &= \frac{50}{|2\vec{a}_x + 7\vec{a}_y + 5\vec{a}_z|} = \frac{50}{\sqrt{2^2 + 7^2 + 5^2}} \\ &= \frac{50}{\sqrt{4 + 49 + 25}} = \frac{50}{\sqrt{78}} = \frac{50}{8.831760866} \\ &= 5.661385171 \text{ V} \approx 5.66 \text{ V AT } A(5\text{m}, 6\text{m}, 7\text{m}) \end{aligned}$$

$$\begin{aligned} V_C &= \frac{Q}{4\pi\epsilon_0 |\vec{r}_C - \vec{r}_B|} \quad \text{WITH } V=0 \text{ AT } \infty \text{ AS REF.} \\ &= \frac{200\pi\epsilon_0}{4\pi\epsilon_0 |(0\vec{a}_x + 0\vec{a}_y + 1\vec{a}_z) - (3\vec{a}_x - 1\vec{a}_y + 2\vec{a}_z)|} \\ &= \frac{50}{|-3\vec{a}_x + 1\vec{a}_y - 1\vec{a}_z|} = \frac{50}{\sqrt{(-3)^2 + 1^2 + (-1)^2}} \\ &= \frac{50}{\sqrt{9 + 1 + 1}} = \frac{50}{\sqrt{11}} = \frac{50}{3.31662479} \\ &= 15.07556723 \text{ V} \approx 15.08 \text{ V AT } C(0\text{m}, 0\text{m}, 1\text{m}) \end{aligned}$$

$$\begin{aligned} V_{AC} &= V_A - V_C = 5.66 \text{ V} - 15.08 \text{ V} \\ &= \underline{\underline{-9.42 \text{ V}}} \quad \text{WITH } V=0 \text{ AT } C \text{ AS REF.} \end{aligned}$$

SOLUTION

$$(2)(b) \quad V_A = -\frac{\rho_L}{2\pi\epsilon_0} \ln \rho \quad \text{WITH } V=0 \text{ AT } \rho=1 \text{ AS REF.}$$

$$= -\frac{40\pi\epsilon_0}{2\pi\epsilon_0} \ln(\sqrt{6^2+7^2})$$

$$= -20 \ln(\sqrt{36+49}) = -20 \ln(\sqrt{85})$$

$$= -20 \ln(9.219544457)$$

$$= -20 \times 2.221325628$$

$$= -44.42651256 \approx -44.43 \text{ V AT A}$$

$$V_c = -\frac{\rho_L}{2\pi\epsilon_0} \ln \rho \quad \text{WITH } V=0 \text{ AT } \rho=1 \text{ AS REF.}$$

$$= -\frac{40\pi\epsilon_0}{2\pi\epsilon_0} \ln(\sqrt{0^2+1^2})$$

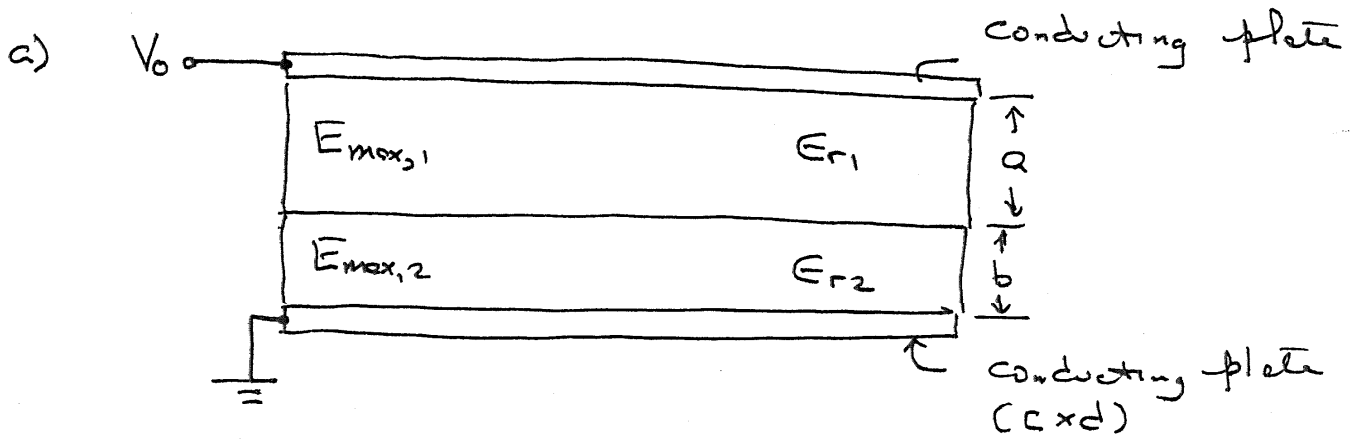
$$= -20 \ln(1)$$

$$= 0 \text{ V AT C}$$

$$V_{AC} = V_A - V_c = -44.43 \text{ V} - 0 \text{ V}$$

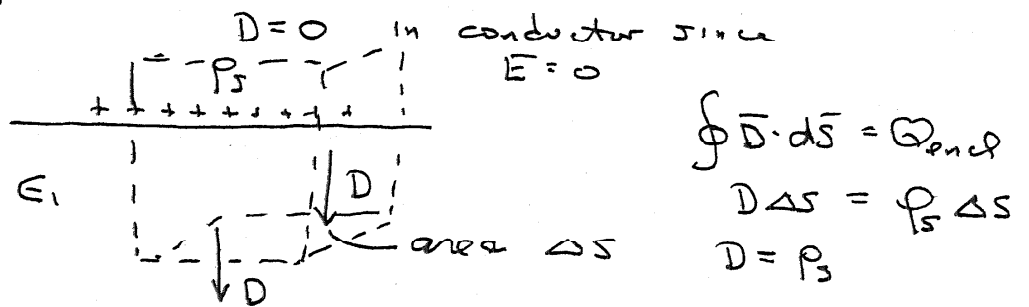
$$= \underline{\underline{-44.43 \text{ V}}} \quad \text{WITH } V=0 \text{ AT C AS REF.}$$

QUESTION 3



$a, b \ll c, d$
 \Rightarrow 1-D geometry
 \Rightarrow 2-layer parallel plate capacitor

b) To determine the electric field in the dielectric regions, it is convenient to use Gauss's Law. The potential V_0 establishes a uniform surface charge density $+\rho_s$ on the lower surface of the upper plate.



Gauss's Law shows that $\vec{D}_1 = \rho_s (-\hat{z}_3)$
 $\vec{D}_2 = \rho_s (-\hat{z}_3)$

But $\vec{E} = \vec{D}/\epsilon \quad \therefore \quad \vec{E}_1 = \frac{P_s}{\epsilon_0 \epsilon_{r1}} (-\hat{a}_z) \quad \text{Mat'l \#1}$

$\vec{E}_2 = \frac{P_s}{\epsilon_0 \epsilon_{r2}} (-\hat{a}_z) \quad \text{Mat'l \#2}$

The question requires \vec{E}_1, \vec{E}_2 in terms of V_0, a, b etc
Using

$$V_0 - 0 = - \int \vec{E} \cdot d\vec{l} = - \int_0^b \vec{E}_2 \cdot d\vec{l} - \int_b^{b+a} \vec{E}_1 \cdot d\vec{l}$$

$$V_0 = \frac{P_s b}{\epsilon_0 \epsilon_{r2}} + \frac{P_s a}{\epsilon_0 \epsilon_{r1}}$$

$$P_s = \frac{V_0 \epsilon_0}{\frac{a}{\epsilon_{r1}} + \frac{b}{\epsilon_{r2}}} = \frac{V_0 \epsilon_0 \epsilon_{r1} \epsilon_{r2}}{a \epsilon_{r2} + b \epsilon_{r1}}$$

and $\vec{E}_1 = \frac{V_0 \epsilon_{r2}}{a \epsilon_{r2} + b \epsilon_{r1}} (-\hat{a}_z)$

$\vec{E}_2 = \frac{V_0 \epsilon_{r1}}{a \epsilon_{r2} + b \epsilon_{r1}}$

c) $Q = 3 \text{mm} \rightarrow 3 \times 10^{-3}$
 $\epsilon_{r1} = 10$
 $E_{\text{max},1} = 70 \times 10^6 \text{ V/m}$

$b = 1 \text{mm} \rightarrow 10^{-3} \text{ m}$
 $\epsilon_{r2} = 6$
 $E_{\text{max},2} = 30 \times 10^3 \text{ V/m}$

$$a \epsilon_{r2} + b \epsilon_{r1} = (3 \times 6 + 1 \times 10) 10^{-3} = 28 \times 10^{-3}$$

V_0 - potential difference across structure
 $V_{0,m1}$ - pot. diff such that $E_1 = E_{\text{max},1}$

$$V_{0,m1} = \frac{70 \times 10^6 \times 28 \times 10^{-3}}{6} = 326.7 \text{ kV}$$

$$V_{0,m2} = \frac{30 \times 10^3 \times 28 \times 10^{-3}}{10} = 84.0 \text{ kV}$$

Clearly, if V_0 is increased from 0, the max. potential difference that can be applied before either region breaks down is

$$| V_{0, \text{max}} = 84 \text{ kV} |$$

(4)

$$(a) \nabla^2 V = -\frac{S_0}{r^2}$$

$$S_0 = -\frac{S_0}{r^2}$$

$$\nabla^2 V = \frac{S_0}{\epsilon_0 r^2}$$

$$(b) \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial V}{\partial r} \right) = \frac{S_0}{\epsilon_0 r^2} \quad \xrightarrow{r \neq 0} \quad \frac{\partial}{\partial r} \left(r^2 \frac{\partial V}{\partial r} \right) = \frac{S_0}{\epsilon_0} \quad \xrightarrow{\text{integrate}} \quad r^2 \frac{\partial V}{\partial r} = \frac{S_0}{\epsilon_0} r + C_1$$

$$\xrightarrow{r \neq 0} \quad \frac{\partial V}{\partial r} = \frac{S_0}{\epsilon_0} \frac{1}{r} + \frac{C_1}{r} \quad \xrightarrow{\text{integrate}} \quad V(r) = \frac{S_0}{\epsilon_0} \ln(r) - \frac{C_1}{r^2} + C_2$$

Boundary conditions: $V(a) = V_0$ $V(b) = 0$

$$\left. \begin{aligned} \frac{S_0}{\epsilon_0} \ln(a) - \frac{C_1}{a} + C_2 &= V_0 \\ \frac{S_0}{\epsilon_0} \ln(b) - \frac{C_1}{b} + C_2 &= 0 \end{aligned} \right\} \frac{S_0}{\epsilon_0} \ln(a/b) + C_1 \left(\frac{1}{b} - \frac{1}{a} \right) = V_0$$

$$C_1 = -\frac{V_0 + \frac{S_0}{\epsilon_0} \ln(b/a)}{1/a - 1/b}$$

$$C_2 = \frac{C_1}{b} - \frac{S_0}{\epsilon_0} \ln(b) = -\frac{(V_0 + \frac{S_0}{\epsilon_0} \ln(b/a))/b}{1/a - 1/b} - \frac{S_0}{\epsilon_0} \ln(b)$$

$$C_2 = -\frac{V_0/b + \frac{S_0}{\epsilon_0} (\ln(b)/a - \ln(a)/b)}{1/a - 1/b}$$

$$V(r) = \frac{S_0}{\epsilon_0} \ln(r) + \frac{V_0 + \frac{S_0}{\epsilon_0} \ln(b/a)}{1/a - 1/b} \frac{1}{r} - \frac{V_0/b + \frac{S_0}{\epsilon_0} (\ln(b)/a - \ln(a)/b)}{1/a - 1/b}$$

$$(c) \underline{E} = -\nabla V = -\hat{r} \frac{\partial V}{\partial r}$$

$$\underline{E}(r) = \left\{ -\frac{S_0}{\epsilon_0} \frac{1}{r} + \frac{V_0 + \frac{S_0}{\epsilon_0} \ln(b/a)}{1/a - 1/b} \frac{1}{r^2} \right\} \hat{r}$$